Coherence and Concentration in Tightly-Connected Networks

Enrique Mallada



Data-based Diagnosis of Networked Dynamical Systems
CCS 2021 Satellite Symposium
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Acknowledgements



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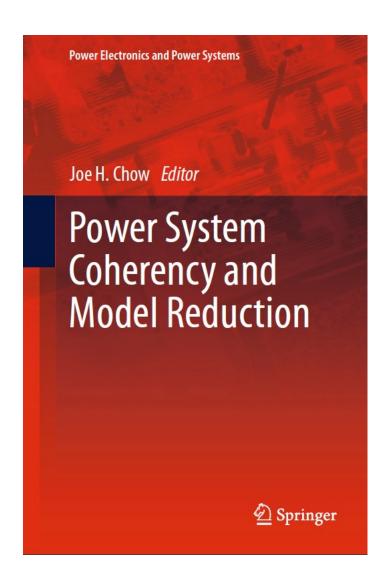




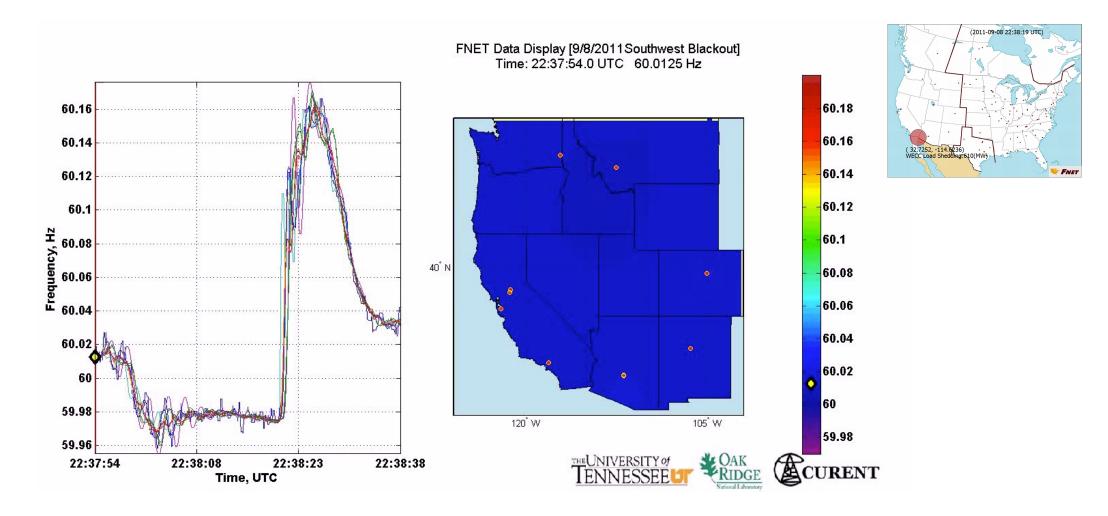


Coherence in Power Networks

- Studied since the 70s
 - Podmore, Price, Chow, Kokotovic, Verghese, Pai, Schweppe,...
- Enables aggregation/model reduction
 - Speed up transient stability analysis
- Many important questions
 - How to identify coherent modes?
 - How to accurately reduce them?
 - What is the cause?
- Many approaches
 - Timescale separations (Chow, Kokotovic,)
 - Krylov subspaces (Chaniotis, Pai '01)
 - Balanced truncation (Liu et al '09)
 - Selective Modal Analysis (Perez-Arriaga, Verghese, Schweppe '82)



This talk



Goals:

- 1. Characterize the coherence response from a frequency domain perspective
- 2. Leverage the coherence response to obtain accurate reduced order models

Coherence and Concentration in Tightly-Connected Networks

Hancheng Min and Enrique Mallada

ArXiv preprint: arXiv:2101.00981

Accurate Reduced-Order Models for Heterogeneous Coherent Generators

Hancheng Min, Fernando Paganini, and Enrique Mallada

IEEE Control Systems Letters, 2021

Storage-Based Frequency Shaping Control

Yan Jiang, Eliza Cohn, Petr Vorobev, Member, IEEE, and Enrique Mallada, Senior Member, IEEE

[TPS 21]

IEEE Transactions on Power Systems, 2021

Grid-forming frequency shaping control

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[L-CSS 21]

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[L-CSS 21]

Outline

- Characterization of Coherent Dynamics [Min, M '21]
- Reduced-Order Model of Coherent Response [Min, Paganini, M '21]

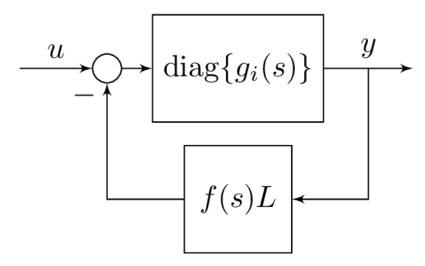
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Coherence in networked dynamical systems

Block Diagram:



Node dynamics: $g_i(s), i = 1, 2, \dots, n$

Symmetric Real Network Laplacian: L

$$L = V\Lambda V^T, \ V = [1/\sqrt{n}, V_{\perp}]$$

 $\Lambda = \text{diag}\{0, \lambda_2(L), \dots, \lambda_n(L)\}$

Coupling dynamics: f(s)

Examples:

Consensus Networks:

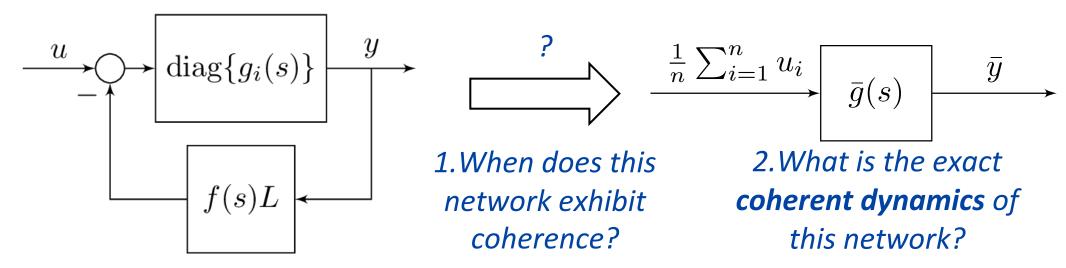
$$g_i(s) = \frac{1}{s}$$
$$f(s) = 1$$

Power Networks (2nd order generator):

$$g_i(s) = \frac{1}{m_i s + d_i + \frac{r_i^{-1}}{\tau_i s + 1}}$$
$$f(s) = \frac{1}{s}$$

Coherence in networked dynamical systems

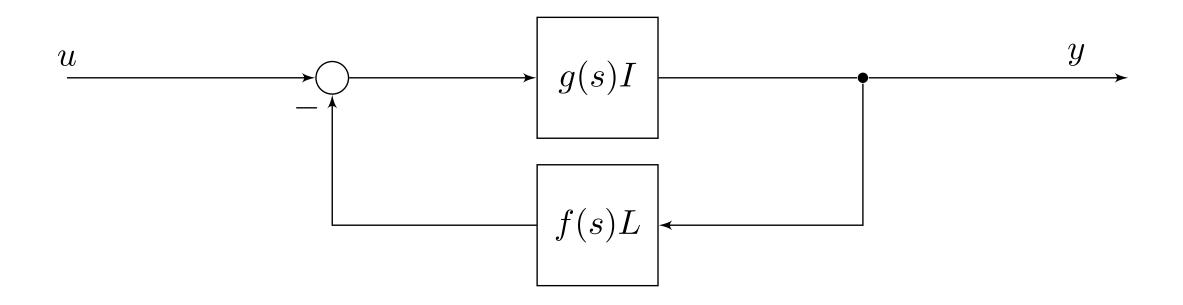
Block Diagram:



- 1. Coherence can be understood as a **low rank** property the **closed-loop transfer matrix**
- 2. It emerges as the **effective algebraic connectivity** increases
- 3. The coherent dynamics is given by the harmonic mean of nodal dynamics

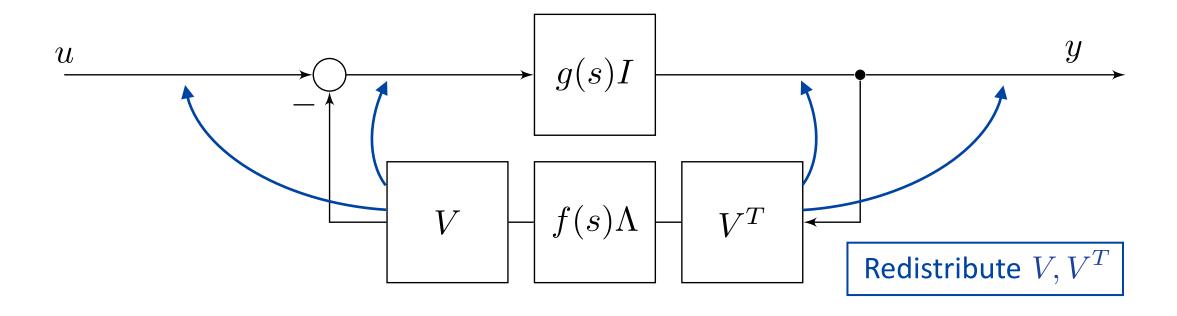
$$\bar{g}(s) = \left(\frac{1}{n} \sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

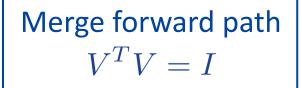
Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$

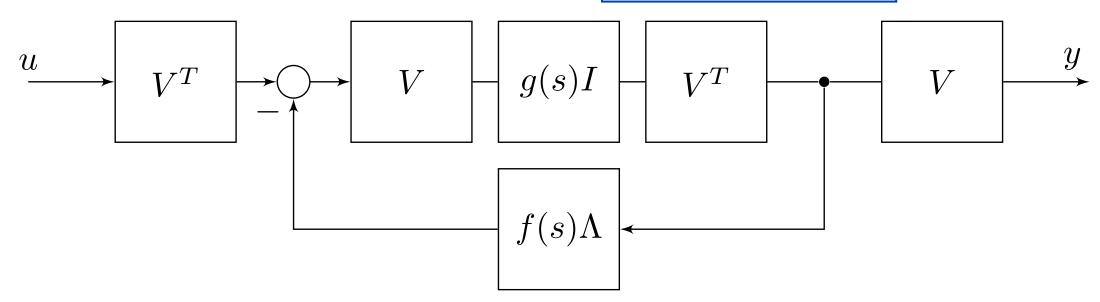


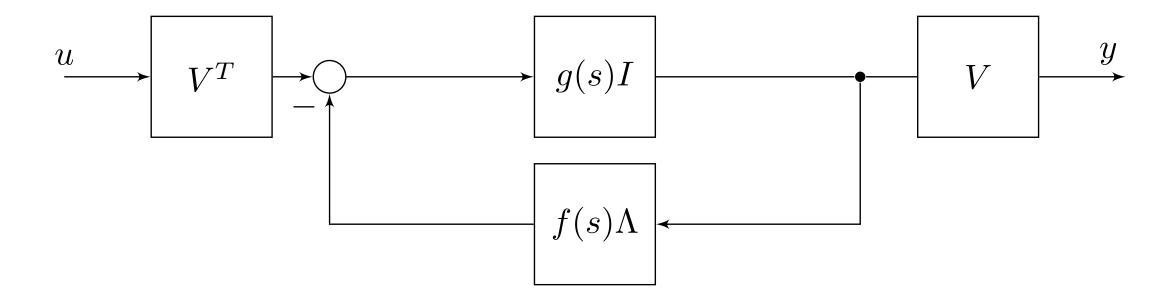
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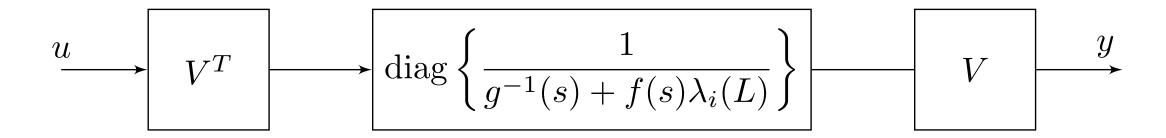
Eigendecomposition $L = V\Lambda V^T$











Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$

The transfer matrix from input u to output y:

$$T(s) = V \operatorname{diag} \left\{ \frac{1}{g^{-1}(s) + f(s)\lambda_i(L)} \right\}_{i=1}^n V^T$$

$$V = [1/\sqrt{n}, V_{\perp}], \ \lambda_1(L) = 0$$

$$T(s) = \frac{1}{n}g(s)\mathbb{1}^{T} + V_{\perp}\operatorname{diag}\left\{\frac{1}{g^{-1}(s) + f(s)\lambda_{i}(L)}\right\}_{i=2}^{n} V_{\perp}^{T}$$

Coherent dynamics independent of the network structure

Dynamics dependent of the network structure

$$T(s) = \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^T + V_{\perp}\operatorname{diag}\left\{\frac{1}{g^{-1}(s) + f(s)\lambda_i(L)}\right\}V^T$$

The effect of non-coherent dynamics vanishes as:

- The algebraic connectivity $\lambda_2(L)$ of the network increases
 - For almost any $s_0 \in \mathbb{C}$

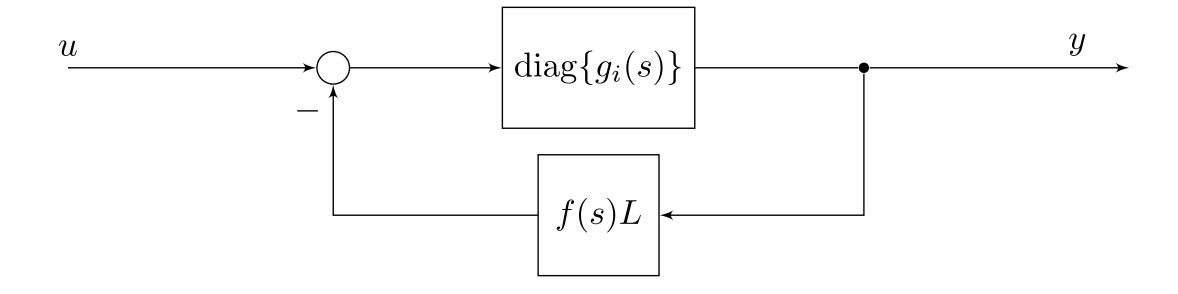
$$\lim_{\lambda_2(L) \to +\infty} \left\| T(s_0) - \frac{1}{n} g(s_0) \mathbb{1} \mathbb{1}^T \right\| = 0$$

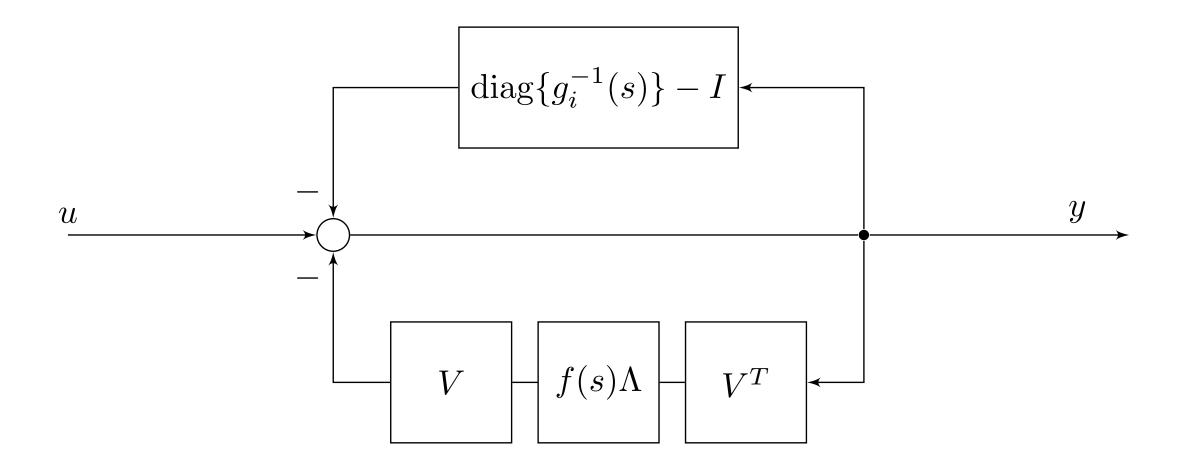
• The point of interest gets close to a **pole** of f(s)

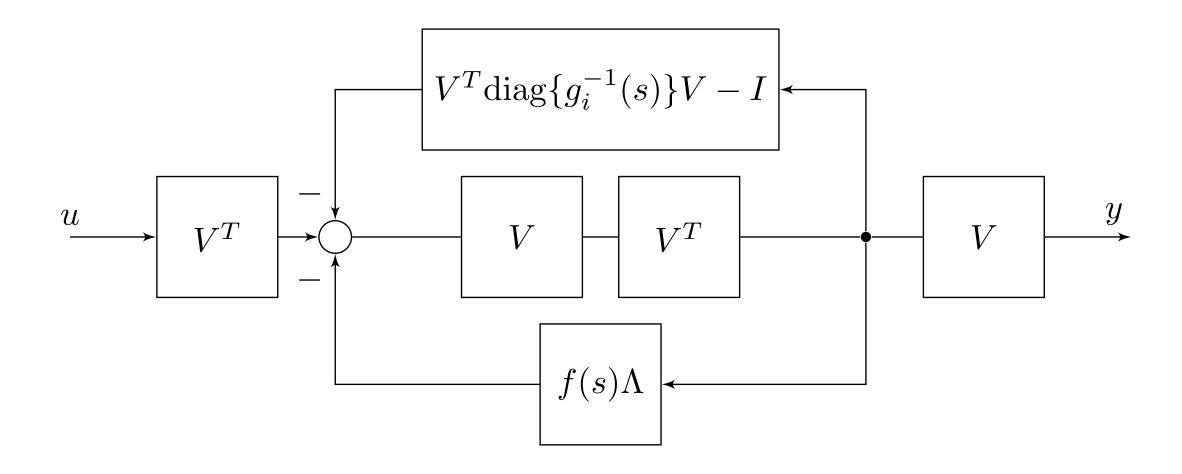
For $s_0 \in \mathbb{C}$, a pole of f(s)

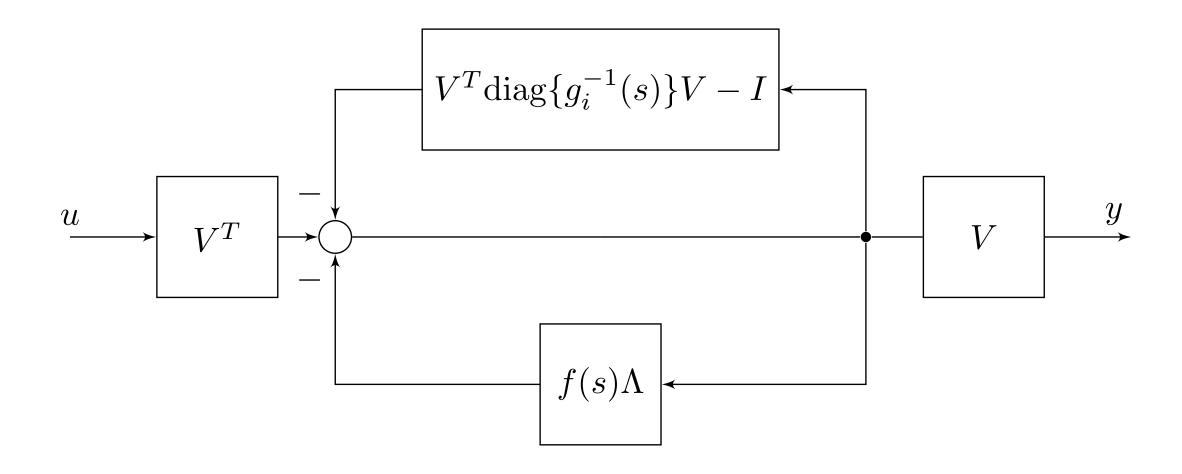
$$\lim_{s \to s_0} \left\| T(s) - \frac{1}{n} g(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

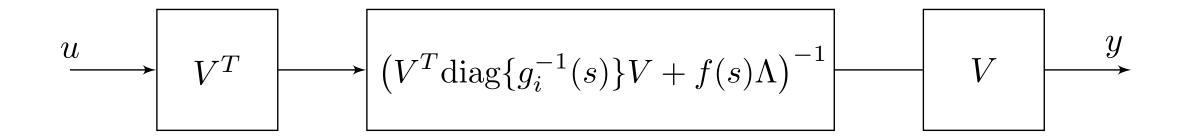
Our frequency-dependent coherence measure $\left\|T(s) - \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^T\right\|$ is controlled by the effective algebraic connectivity $|f(s)|\lambda_2(L)$











The transfer matrix from input u to output y:

$$T(s) = V \left(V^T \operatorname{diag} \{ g_i^{-1}(s) \} V + f(s) \Lambda \right)^{-1} V^T$$

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The transfer matrix from input u to output y:

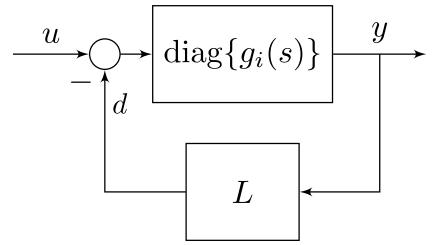
$$T(s) = V \left(V^T \operatorname{diag}\{g_i^{-1}(s)\}V + f(s)\Lambda \right)^{-1} V^T$$

$$T(s) = \begin{bmatrix} \frac{1}{n} \bar{g}(s) \mathbb{1} \mathbb{1}^T \\ N(s) \end{bmatrix} + \begin{bmatrix} N(s) \\ Network \\ Network$$

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Informed guess for coherent dynamics: $\overline{g}(s)$

Block Diagram:



Coherent Dynamics:

$$\bar{y}(s) = \left(\frac{1}{n}\sum_{i=1}^n g_i^{-1}(s)\right)^{-1} \frac{1}{n}\sum_{i=1}^n u_i(s) \left| \begin{array}{c} \text{Average equations from } i=1 \text{ to } n: \\ \text{Average equations from } i$$

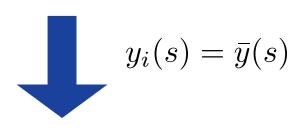
$$\bar{g}(s) = \left(\frac{1}{n} \sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

Harmonic mean of all $g_i(s)$

Dynamics for node *i*

$$y_i(s) = g_i(s)(u_i(s) - d_i(s)), i = 1, \dots, n$$

Assume all nodes output are **identical** as the result of coherence



$$g_i^{-1}(s)\bar{y}(s) = u_i(s) - d_i(s), \ i = 1, \dots, n$$

$$\left(\frac{1}{n}\sum_{i=1}^{n}g_{i}^{-1}(s)\right)\bar{y}(s) = \frac{1}{n}\sum_{i=1}^{n}u_{i}(s) - \left[\frac{1}{n}\sum_{i=1}^{n}d_{i}(s)\right]$$

 $\mathbb{1}^T L = \mathbb{0}$

$$T(s) = \frac{1}{n}\bar{g}(s)\mathbb{1}\mathbb{1}^T + T(s) - \frac{1}{n}\bar{g}(s)\mathbb{1}\mathbb{1}^T$$

$$\bar{g}(s) = \left(\frac{1}{n} \sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

The effect of non-coherent dynamics vanishes as:

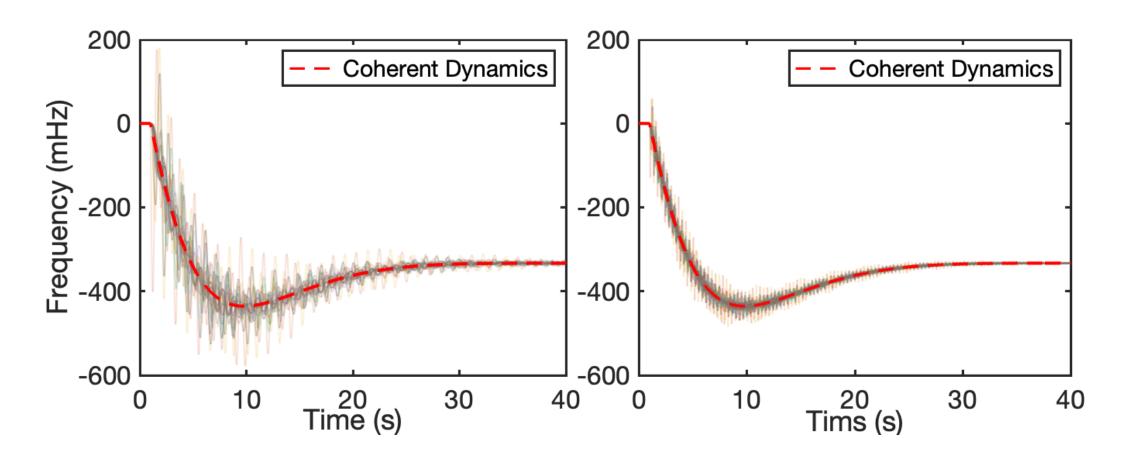
• For almost any $s_0 \in \mathbb{C}$

$$\lim_{\lambda_2(L) \to +\infty} \left\| T(s_0) - \frac{1}{n} \bar{g}(s_0) \mathbb{1} \mathbb{1}^T \right\| = 0 \qquad \lim_{s \to s_0} \left\| T(s) - \frac{1}{n} \bar{g}(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

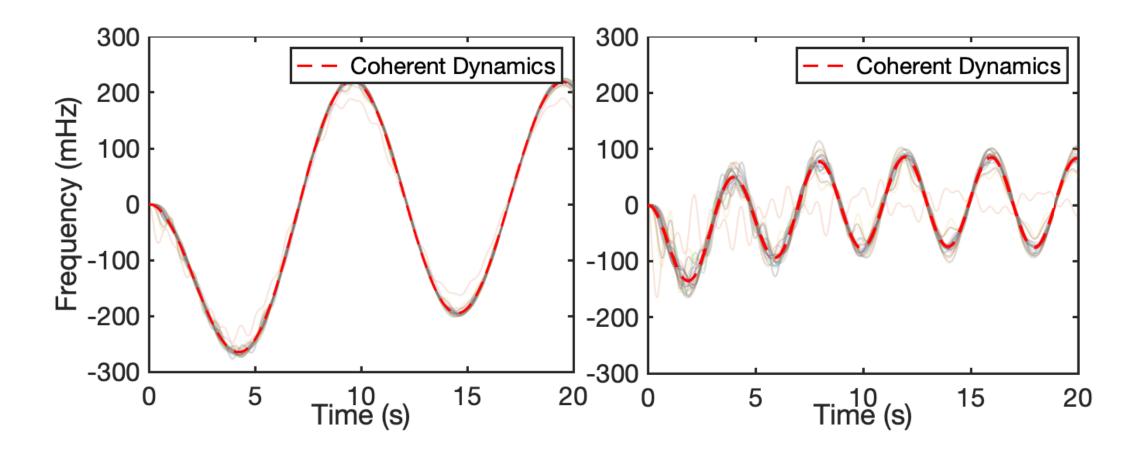
• For $s_0 \in \mathbb{C}$, a pole of f(s)

$$\lim_{s \to s_0} \left\| T(s) - \frac{1}{n} \overline{g}(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

- Excluding zeros: the limit holds at zero, but by different convergence result
- We can further prove uniform convergence over a compact subset of complex plane, if it doesn't contain any zero nor pole of $\bar{g}(s)$
- Convergence of transfer matrix is **related to time-domain response** by Inverse Laplace Transform
- Extensions for random network ensembles $\bar{g}(s) = (E_w[g^{-1}(s, w)])^{-1}$



Coherent dynamics acts as a more accurate version of the Center of Inertia (CoI)



Outline

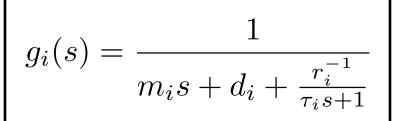
- Characterization of Coherent Dynamics [Min, M '21]
- Reduced-Order Model of Coherent Response [Min, Paganini, M '21]

Accurate Reduced-Order Models for Heterogeneous Coherent Generators

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IEEE Control Systems Letters, 2021

Aggregation of Coherent Generators

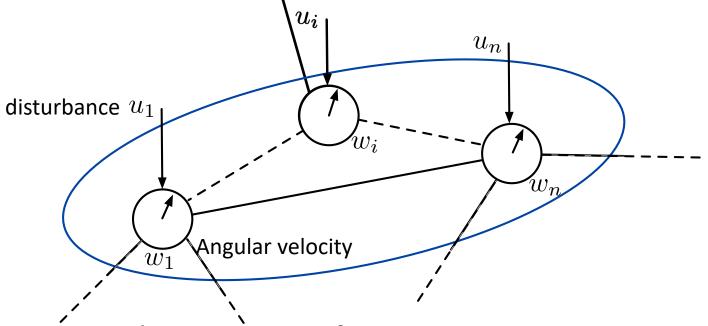


 m_i : inertia

 d_i : damping coefficient

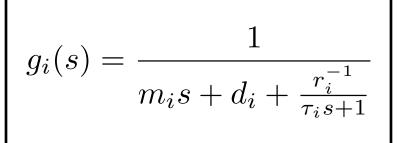
 r_i^{-1} : droop coefficient

 τ_i : turbine time constant

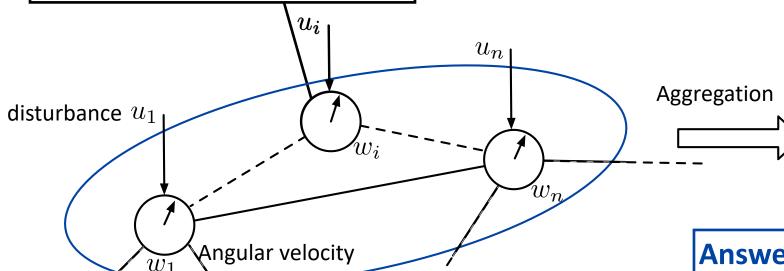


coherent group of n generators

Aggregation of Coherent Generators



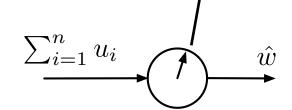
Question: How to choose the different parameters of $\hat{g}(s)$?



coherent group of n generators

$$\hat{g}(s) = \frac{1}{\hat{m}s + \hat{d} + \frac{\hat{r}^{-1}}{\hat{\tau}s + 1}}$$

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Answer: Use instead

$$\hat{g}(s) = \frac{1}{n}\bar{g}(s) = \left(\sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

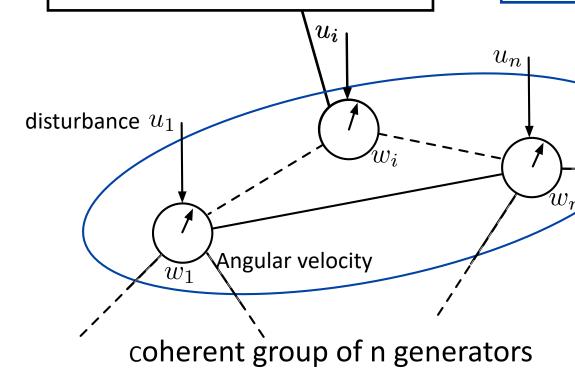
Aggregation for Homogeneous $au_i = au$

$$g_i(s) = \frac{1}{m_i s + d_i + \frac{r_i^{-1}}{\tau_i s + 1}}$$

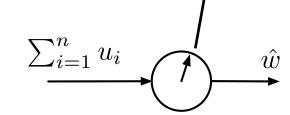
then
$$\hat{m} = \sum_{i=1}^{n} m_i$$
, $\hat{d} = \sum_{i=1}^{n} d_i$, $\hat{r}^{-1} = \sum_{i=1}^{n} r_i^{-1}$

suppose $au_i = au$

Aggregation



$$\hat{g}(s) = \frac{1}{\hat{m}s + \hat{d} + \frac{\hat{r}^{-1}}{\hat{\tau}s + 1}}$$



$$\hat{g}(s) = \frac{1}{(\sum_{i=1}^{n} m_i)s + (\sum_{i=1}^{n} d_i) + \frac{1}{\tau s + 1}(\sum_{i=1}^{n} r_i^{-1})}$$

Challenges on Aggregating Coherent Generators

For generator dynamics given by a swing model with turbine control:

$$g_i(s) = rac{1}{m_i s + d_i + rac{r_i^{-1}}{ au_i s + 1}}$$

The aggregate dynamics:

Need to find a low-order approximation of $\hat{g}(s)$

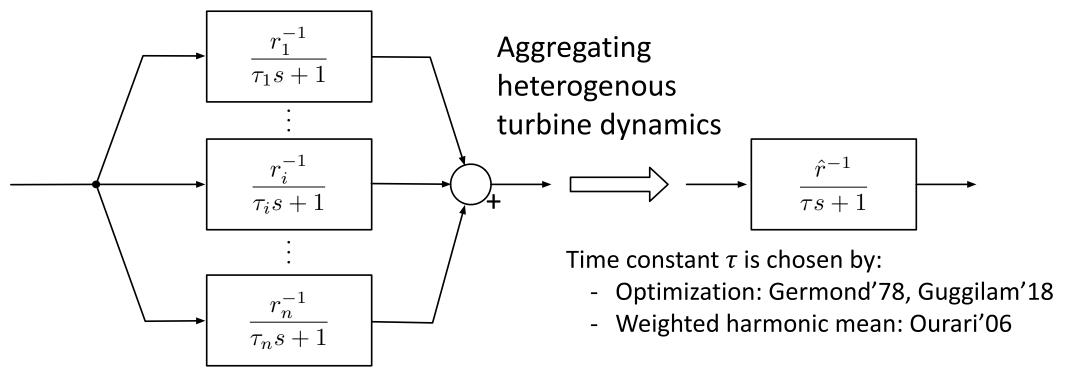
$$\hat{g}(s) = \frac{1}{\hat{m}s + \hat{d} + \sum_{i=1}^{n} \frac{r_i^{-1}}{\tau_i s + 1}}$$

high-order if τ_i are heterogeneous

Enrique Mallada (JHU)

Prior Work: Aggregation for heterogeneous τ_i s

When time constants are **heterogenous**:



Drawbacks:

- the order of overall approximation model is restricted to 2nd order
- the only "decision variable" is the time constant
- does not consider the effect of inertia or damping in the approx.

Inaccurate Approximation

Balanced Truncation

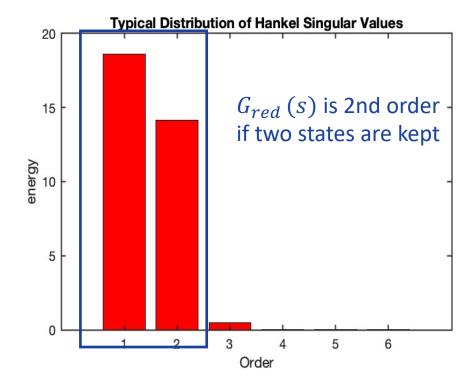
A model reduction method on stable system G(s) such that:

- The reduced model $G_{red}(s)$ is stable
- The error in H_{∞} -norm:

$$\|G(s) - G_{red}(s)\|_{\mathcal{H}_{\infty}}$$

is upper bounded by a small value that depends on G(s) and the order of $G_{red}(s)$

k-th order $G_{red}(s)$ is obtained by only keeping states of G(s) associated with k largest Hankel Singular Value



There is DC gain mismatch between G(s) and $G_{red}(s)!!$

Frequency Weighted Balanced Truncation

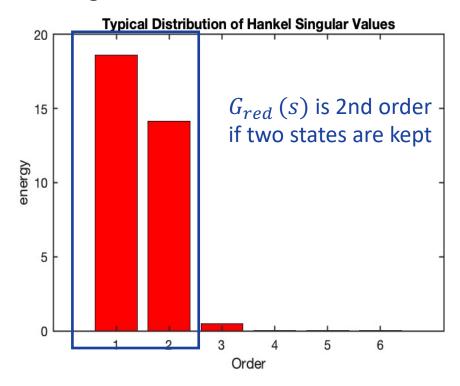
A frequency weighted model reduction method on stable system G(s) such that:

- The reduced model $G_{red}(s)$ is stable
- The frequency weighted error in H_{∞} -norm:

$$||W(s)(G(s) - G_{red}(s))||_{\mathcal{H}_{\infty}}$$

is upper bounded by a small value that depends on G(s) and the order of $G_{red}(s)$) and W(s)

k-th order $G_{red}(s)$ is obtained by only keeping states of G(s) associated with k largest frequency weighted Hankel Singular Value



The DC gain mismatch between G(s) and $G_{red}(s)$ can be made arbitrarily small weighting higher low freqs.

Aggregation Model by Frequency Weighted Balanced Truncation

Two approaches to get a k-th order reduction model of aggregate dynamics $\hat{g}(s)$:

• (k-1)-th order balanced truncation on high-order turbine dynamics

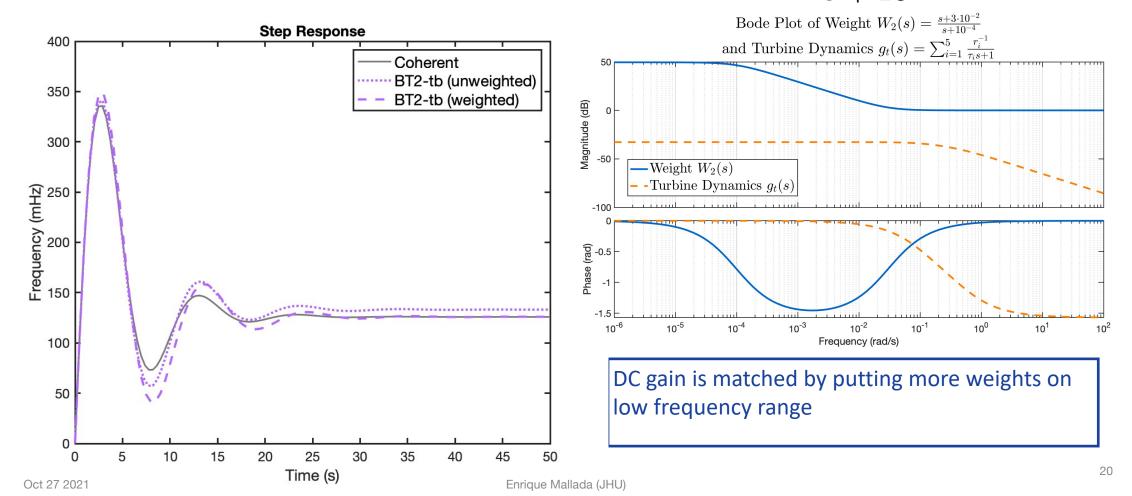
$$\tilde{g}_k^{tb}(s) = \frac{1}{\hat{m}s + \hat{d} + \underbrace{\tilde{g}_{t,k-1}(s)}}$$
 (k-1)-th reduction model on $\sum_{i=1}^n \frac{r_i^{-1}}{\tau_i s + 1}$

ullet k-th order balanced truncation on closed-loop dynamics $\hat{g}(s)$

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Numerical Simulation—Matching DC Gain in Balanced Truncation

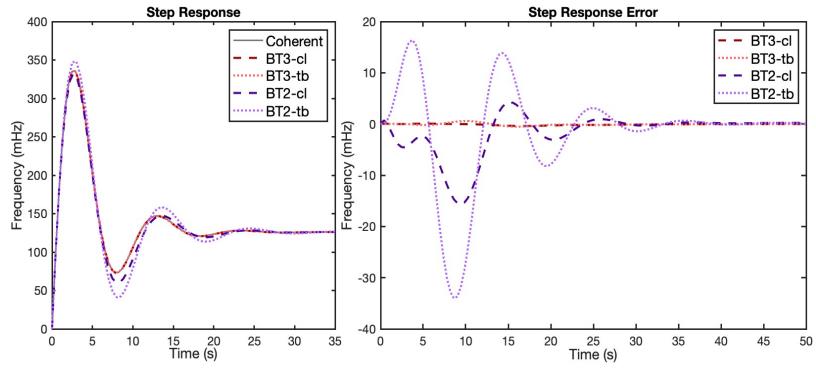
Compare 2nd order model by balanced truncation on turbine dynamics with different weights: $W_1(s)=1$ (unweighted) $W_2(s)=\frac{s+3\cdot 10^{-2}}{s+10^{-4}}$ (weighted)



Numerical Simulation—Compare Models by Balanced Truncation

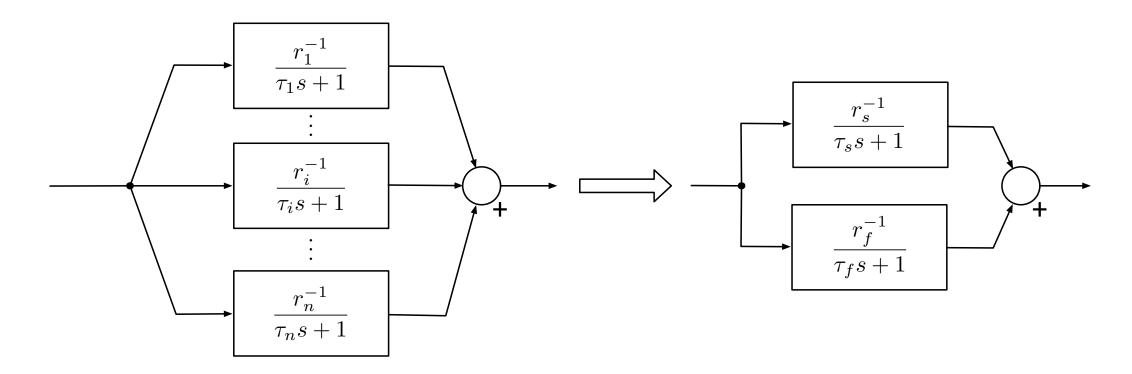
We compare the following 4 reduced order models:

- Balanced truncation on **turbine** dynamics with weight $W_{tb}(s) = \frac{s+3\cdot 10^{-2}}{s+10^{-4}}$
 - 2nd order (BT2-tb)
 - 3rd order (BT3-tb)
- Balanced truncation on closed-loop dynamics with weight $W_{cl}(s) = \frac{s+8\cdot 10^{-2}}{s+10^{-4}}$
 - 2nd order (BT2-cl)
 - 3rd order (BT3-cl)



- 3rd order models are almost accurate
- balanced truncation on closed-loop is better than on turbine dynamics, given the same order

Interpretation of 3rd Order Reduced Model



- The high-order turbine dynamics can be almost accurately recovered by two turbines in parallel
- Such approximation works for aggregating even more turbines than in the test case

Summary

 Frequency domain characterization of coherent dynamics, as a low rank property of the transfer function.

- Coherence is a frequency dependent property:
 - Effective algebraic connectivity $f(s)\lambda_2(L)$
 - Disturbance frequency spectrum
- We use frequency weighted balanced truncation to suggest possible improvements to obtain accurate reduced order model of aggregated dynamics of coherent generators:
 - increase model complexity (3rd order/two turbines)
 - model reduction on closed-loop dynamics

Thanks!

Related Publications:

- Min, M, "Coherence and Concentration in Tightly Connected Networks," submitted
- Min, Paganini, M, "Accurate Reduced Order Models for Coherent Synchronous Generators," L-CSS 2021
- Jiang, Bernstein, Vorobev, M, "Grid-forming Frequency Shaping Control," L-CSS 2021





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